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TITLE OF THE INVENTION

MOTOR POWER SUPPLY CONTROL APPARATUS

CROSS-REFERENCE TO RELATED APPLICATION

[0001] This application claims the benefit of Korean Patent Application No. 2003-31125, filed May 16, 2003, in the Korean Intellectual Property Office, the disclosure of which is incorporated herein by reference.

BACKGROUND OF THE INVENTION

1. Field of the Invention

[0002] The present invention relates to a power supply device for a motor, and more particularly, to a motor power supply device which reduces a redundant usage of components by sharing a dynamic braking circuit and an inverter, resulting in a reduction in sizes of products and a manufacturing expense thereof and further provides a satisfactory value of resistance for motor speed of a break circuit.

2. Description of the Related Art

[0003] A three-phase motor has a coil wired in a triangle shape and a power supply device for the three-phase motor generates a three-phase voltage to operate the motor. As shown in FIG. 1, the three-phase motor power supply comprises a AC (Alternating Current) power supply part 101 supplying 110V/220V commercial AC power; a rectifier 103 rectifying the AC power generated from the AC power supply part 101 to a DC power; a capacitor 115 smoothing out the rectified voltage in the rectifier 103; an inverter 116 inverting the DC power from the capacitor

115 to a AC power having various frequencies and generating a three-phase voltage. The inverter 116 has a plural number of transistors turned on/off depending on a PWM (Pulse Width Modulation) control signal, and diodes connected in parallel with each of the plural number of transistors. The three-phase motor power supply further comprises a microprocessor (not shown) turning on/off the transistors of the inverter 116, responding to the PWM control signal and modulating power frequencies to control a rotation speed of an AC motor 117.

[0004] A motor power supply device generally comprises an inrush-current protection circuit formed to consume inrush-current flowing from an inrush-current resistor 102 to the capacitor 115 by turning off a relay 111 for inrush-current protection when an initial power is applied; an over voltage protection circuit 130, connected across the inverter 116, protecting the capacitor 115 from an over-voltage condition and including an over voltage protection resistor 112 and a diode 113 connected, in parallel, in series with a control switching element 114; and a dynamic braking circuit shortening power input terminals of the AC motor 117.

[0005] The dynamic braking circuit has dynamic braking resistors 120 connected with a braking relay 122 across each pair of power input terminals U and V; U and W of the AC motor 117.

[0006] As shown in FIG. 2, the three-phase motor power supply comprises a AC (Alternating Current) power supply part 201 supplying 110V/220V commercial AC power; a rectifier 203 rectifying the AC power generated from the AC power supply part 201 to a DC power; a capacitor 215 smoothing out the rectified voltage in the rectifier 203; an inverter 216 inverting the DC power from the capacitor 215 to a AC power having various frequencies and generating a three-phase voltage. The inverter 216 has a plural number of transistors 254b turned on/off

depending on a PWM (Pulse Width Modulation) control signal, and diodes connected in parallel with each of the plural number of transistors 254b. The three-phase motor power supply further comprises a microprocessor (not shown) turning on/off the transistors 254b of the inverter 216, responding to the PWM control signal and modulating power frequencies to control a rotation speed of an AC motor 217.

[0007] A motor power supply device generally comprises an inrush-current protection circuit formed to consume inrush-current flowing from an inrush-current resistor 202 to the capacitor 215 by turning off a relay 211 for inrush-current protection when an initial power is applied; and a dynamic braking circuit 230 to brake the AC motor 217.

[0008] The dynamic braking circuit, as shown in FIG. 2, having pairs of dynamic braking diodes 224, respectively, connected to each of the power input terminals of the AC motor 217. Further the respective dynamic braking diodes 224 may be parallel connected to a dynamic braking resistor 220 and a braking relay 222.

[0009] Further, as shown in FIGS. 1 or 2, the braking relay 122 or 222 stays in an off state when the AC motor 117 or 217 is in a driving mode, and the braking relay 122 or 222 is turned on when the motor 117 or 217 is about to stop or after the AC motor 117 or 217 is stopped. When the braking relay 122 or 222 is activated, the AC motor 117 or 217 stops suddenly or prevents the AC motor 117 or 217 from rotating due to an external force.

[0010] However, the dynamic braking circuit only operates while the AC motor 117 or 217 is stopping or after the motor 117 or 217 is stopped in the conventional dynamic braking circuit. The dynamic braking circuit does not operate while the AC motor 117 or 217 is regularly in the driving mode when power is supplied and the capacitor 115 or 215 is charged with the power.

However, the dynamic braking circuit is independently provided with components to perform an operation as required, resulting in an increase in a size of an entire circuit and an increase in an expense for a manufacture thereof.

[0011] A size of the dynamic braking resistor 120 or 220 depends on amounts of current flowing through the shortcircuited AC motor 117 or 217, and the amounts of the currents therein depend on a preceding speed when the AC motor 117 or 217 is about to stop. Thus, a resistance value of the dynamic braking resistor 120 or 220 is increased as the AC motor 117 or 217 rotating at high speed tries to stop. The resistance value of the dynamic braking resistor 120 or 220 is decreased as the motor rotating at slow speed tries to stop. Therefore, a motor speed may determine the resistance value of the dynamic braking resistor 120 or 220.

However, the conventional AC motor 117 or 217 was not designed in consideration of such a configuration.

[0012] Thus, the present invention provides a motor power supply in which a number of elements of a dynamic braking circuit and an inverter share a diode and also reduce a size of products and a manufacturing expense thereof. Further, with an effect that a value of resistance in a braking mode is variable depending on a motor speed, a satisfactory value of resistance for a braking circuit is provided.

SUMMARY OF THE INVENTION

[0013] The above described aspects are achieved by providing a motor power supply comprising a DC power supply part having a pair of power supply parts; a pair of connection terminals connected to the pair of power supply parts of each DC power supply part; and an inverter absorbing the DC power from the DC power supply part and supplies an AC power to

the motor. The motor power supply further comprises a braking resistor disposed inside of additional lines interconnecting each of the connection terminals; a control switching element having a series connection with the braking resistor; a braking switch engaging with one of the connection terminals and switched to either a normal position connecting the one connection terminal to a corresponding power supply terminal or a braking position connecting the connection terminal to a corresponding additional line; a motor speed detector detecting a motor speed; a control part controlling the braking switch to switch to the braking position, controlling an on-off interval of the control switching element depending on the motor speed detected by the motor speed detector.

[0014] Further, the motor power supply according to the present invention further comprises an over voltage protection resistor having a first side connected between the braking resistor and the control switching element and a second side connected to one of the connection terminals to connect the over voltage protection resistor and the control switching element connected in series; a capacitor disposed inside of the DC power supply part, applying the voltage generated from the motor; an over voltage detector detecting an over voltage applied on opposite sides of the capacitor. The control part may control the braking switch to switch to the normal position when the over voltage detector detects the over voltage on the opposite sides of the capacitor and to turn on the control switching element resulting in the motor power supply operating the over voltage protection. The control switching element may be shared by the over voltage protection and the dynamic braking.

[0015] The motor power supply further comprises a diode connected, in parallel, with an over voltage protection resistor, and the diode may have a cathode connected to the connection terminal of the inverter allowing a current to flow through the over voltage protection resistor

when the control switching element is turned off.

[0016] Further, the control part controls the braking switch to switch to the normal position when the motor is in a driving mode to activate the motor in a different mode such as a control mode, an over voltage mode, and a dynamic braking mode, respectively, corresponding to a switching position of the braking switch.

[0017] The braking resistor may have a smaller resistance value than that of the over voltage protection resistor so that a majority of the currents flow through the break resistor when the motor is in a dynamic braking mode.

[0018] The braking switch may comprise a relay including a first contact point where the braking switch switches to the normal position; and a second contact point where the braking switch switches to the braking position, and having the first and the second contact points switchable therebetween.

[0019] Additional aspects and/or advantages of the invention will be set forth in part in the description which follows and, in part, will be obvious from the description, or may be learned by practice of the invention.

[0020] The above and/or other aspects of the present invention are achieved by providing a motor power supply including a DC power supply part having a pair of power supply terminals, and an inverter having a pair of connection terminals, respectively, connected to the pair of power supply terminals of the DC power supply part to receive DC power from the DC power supply part and to supply AC power to a motor, and the motor power supply comprising a braking resistor disposed in an additional line connecting the pair of connection terminals to

each other a control switching element disposed with the braking resistor, in parallel, in the additional line a braking switch disposed to one of the pair of connection terminals and switched to either a normal position connecting the one connection terminal to a corresponding power supply part, or a braking position connecting the one connection terminal to the additional line a motor speed detector detecting a speed of the motor and a control part controlling the braking switch to be switched to the braking position and controlling the control switching element so that an on-off interval of the control switching element is controllable depending on the detected speed by the motor speed detector.

[0021] According to an aspect, the motor power supply further comprises an over voltage protection resistor having a first side connected between the braking resistor and the control switching element, and a second side connected to one of the connection terminals to place in series with the control switching element; a capacitor disposed in the DC power supply part and receiving a voltage from the motor; and an over voltage detector detecting an over voltage passed to opposite ends of the capacitor, and the control part controls the braking switch to switch to the normal position and turns the control switching element on when the over voltage detector detects the over voltage on the opposite ends of the capacitor.

[0022] According to an aspect, the motor power supply further comprises a diode disposed, in parallel, with an over voltage protection resistor, having a cathode connected to the connection terminal of the inverter to which the over voltage protection resistor is connected.

[0023] According to an aspect, the control part controls the braking switch to switch to the normal position when the motor is in the driving mode.

[0024] According to an aspect, the braking resistor is smaller in a resistance value than that

of the over voltage protection resistor.

[0025] According to an aspect of the invention, the braking switch is a relay having a first contact point where the braking switch switches to the normal position and a second contact point where the braking switch switches to the braking position.

BRIEF DESCRIPTION OF THE DRAWINGS

[0026] These and/or other aspects and advantages of the present invention will become apparent and more readily appreciated from the following description of the embodiment, taken in conjunction with the accompany drawings of which:

[0027] FIGS. 1 and 2 are circuit diagram of conventional motor power supply devices;

[0028] FIG. 3A is a circuit diagram of a motor power supply device according to an embodiment of the present invention;

[0029] FIG. 3B is a block diagram of a motor power supply device according to the embodiment of the present invention;

[0030] FIG. 4 is a circuit diagram of currents flow when the motor in FIG. 3 is in a control mode;

[0031] FIG. 5 is a circuit diagram of currents flow when the motor in FIG. 3 is in an over voltage protection mode;

[0032] FIGS. 6A-6C illustrate waveforms of a current and a voltage of each contact point of the motor power supply device;

[0033] FIG. 7 is a circuit diagram of currents flow when the motor in FIG. 3 is in a dynamic braking mode;

[0034] FIGS. 8A-8B are graphs illustrating a duty ratio of a control switching element and dynamic braking current I_{DB} depending on a motor speed;

[0035] FIG. 8C illustrates an equivalent circuit of a control switching element duty ratio;

[0036] FIG. 9 shows a simplified equivalent circuit diagram of FIG.3.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

[0037] Reference will now made in detail to the embodiment of the present invention, examples of which are illustrated in the accompanying drawings, wherein like reference numerals refer to the like elements throughout. The embodiment is described below in order to explain the present invention by referring to the figures.

[0038] FIG. 3A illustrates a circuit of a motor power supply according to an embodiment of the present invention. As illustrated in FIG. 3A, the motor power supply comprises a DC power supply part 20 receiving AC power from an AC power supply part 10 and supplying DC power through a pair of power supply terminals 80a and 80b; and an inverter 30 receiving the DC power from the DC power supply part 20 through a pair of connection terminals 90a and 90b which are, respectively, connected to the pair of power supply terminals 80a and 80b and converting the DC power into AC power having various frequencies so as to supply a three-phase voltage to an AC motor 40.

[0039] The motor power supply comprises a braking resistor 56 and a control switching element 58 serially disposed in an additional line connectable with the pair of power supply

terminals 80a and 80b of the inverter 30, having series connection with the connection terminal 90 of the inverter 30 each other; a braking switch 60 to connection terminal 90A the connection terminal 90a to the respective power supply part 80a or to the additional line; an over voltage protection resistor 54 connected in series with the control switching element 58, having a side connected to the connection terminal 90a of the inverter 30 and a remaining side connected between the braking resistor 56 and the control switching element 58; a diode 52 connected, in parallel, with the over voltage protection resistor 54, having a cathode connected to the connection terminal 90a of the inverter 30 to which the over voltage protection resistor 54 is connected; a motor speed detector 99 (see FIG. 3B) detecting a speed the of AC motor 40; and a control part (see FIG. 3B) controlling, the control switching element 58 and the braking switch 60.

[0040] The DC power supply part 20 includes a rectifier 26 rectifying the AC power supplied from the AC power supply part 10, and a capacitor 28 smoothing out the rectified AC power from the rectifier 26. An inrush-current protection circuit is provided inside of the DC power supply part 20 to prevent a large amount of inrush-current from being generated to charge the capacitor 28 on the initial power supply.

[0041] The inrush-current protection circuit has an inrush-current protection resistor 24 consuming a current inrushing into the capacitor 28, transforming the inrush-current into a form of heat energy; and an inrush-current protection relay 22 turned off so that a rectified voltage in the rectifier 26 is transferable to the capacitor 28 by passing through the inrush-current protection resistor 24, or turned on so that the rectified voltage is transferable to the capacitor 28 without passing through the inrush-current protection resistor 24.

[0042] The control part (to be described later) prevents the capacitor 28 from being damaged by turning off the inrush-current protection relay 22 so that the inrush-current may be consumed by the inrush-current protection resistor 24 when the power is initially applied from the AC power supply part 10. Further, a voltage (V_{pn}) between opposite ends of the capacitor 28 increases slowly as the capacitor 28 charges.

[0043] The inverter 30 has several inverting elements 32 formed in a pair of a transistor 32b and a diode 32a in a parallel connection thereof. Further, each power input terminal U, V and W of the AC motor 40 is, respectively, connected between corresponding pairs of the inverting elements 32 and supplied a three-phase voltage by the inverter 30 so as to input the three-phase voltage from the inverter 30.

[0044] Similar to a MOS Transistor or a Field Effect Transistor, the control switching element 58 is switchable depending on an input signal on a gate, and the control part controls the input signal to the control switching element 58 so as to turn on/off the control switching element 58, and changing an interval between a turning on and a turning off of the control switching element 58.

[0045] The motor speed detector 99 may be an encoder coding an angle of a rotation position of the AC motor 40 and calculating a position and a speed of the AC motor 40 based on an encoded signal. The encoder may provide the control part with information of the speed and the angle of the rotation position of the AC motor 40.

[0046] The braking switch 60 may be a relay having a first contact point ① and a second contact point ② through which the connection terminal 90a of the inverter 30 is selectively connectable to one of the power supply part 80a (the normal position) and the additional line (i.e., the braking position).

[0047] After the initial power is applied and a predetermined time passes, opposite ends of the capacitor 28 are completely charged and then a motor activating signal is generated by external operations. Once the motor activating signal is generated, the control part switches the braking switch 60 to connect to the first contact point ① (i.e., the normal position). Further, as shown in FIG. 4, the voltage charging the capacitor 28 is supplied to the inverter 30 and the inverter 30 transforms the applied DC power to a three-phase AC voltage for the AC motor 40.

[0048] While the AC motor 40 is in a driving mode in the above process, however, rotational energy stored by the AC motor 40 regenerates in the capacitor 28 through the inverter 30. Such a regenerative voltage increases the voltage (V_{pn}) between the opposite ends of the capacitors 28.

[0049] When an over voltage detector (not shown) detects an over-voltage condition on the opposite ends of the capacitor 29, the control part keeps the braking switch 60 connected to the first contact point ①, turning on the control switching element 58. Further, the over-voltage is transformed to heat and consumed by the over voltage protection resistor 54 preventing the capacitor 28 from being damaged, and if there is no over-voltage detected, the control part turns off the control switching element 58 so that the current bypass the over voltage protection resistor 54 and flows through the diode 52 (refer to FIG. 5).

[0050] As shown in FIGS. 6A-6C, if the voltage between the opposite ends of the capacitor

28 reaches a maximum limit of over voltage V_{H2} while an over voltage area is in a hysteresis range V_{H1} - V_{H2} , the control part keeps the braking switch 60 connected to the first contact point ① and turns the control switching element 58 on to allow the over voltage to be transformed to heat and consumed by the over voltage protection resistor 54. Thus, the voltage between the opposite ends of the capacitor 28 is decreased.

[0051] The control part controls the control switching element 58 so that a variation of the voltage applied to the opposite ends of the capacitor 28 is limitable within the over voltage range (i.e., hysteresis range, V_{H1} - V_{H2}) (refer to FIGS. 6A-6C), and operates the control switching element 58 within the hysteresis range V_{H1} - V_{H2} to decrease a malfunctioning of the control switching element 58 due to noises.

[0052] The control part connects the braking switch 60 to the second contact point ② and turns off the transistor 32b of the inverter 30 when the AC motor 40 makes a sudden stop or the AC motor 40 stops driving when power is not applied. The control part enters control signals into a gate of the control switching element 58, and the control signal controls the on-off interval of the control switching element 58 depending on a result of the motor speed detector 99.

[0053] Thus, a portion of the current flowing in winding wires around the AC motor 40 flows into the AC motor 40 through the diode 32a of the inverter 30 and the braking resistor 56 resulting in shortening of the power connection terminals, and the braking resistor 56 consumes the current transformed into the heat. A further portion of the current flowing in the winding wires around the AC motor 40, flows in the over voltage protection resistor 54 connected with the braking resistor 56, in parallel, but the over voltage protection resistor 54 generally has a larger resistance value than that of the braking resistor 56, consequently the currents mostly

flow through the braking resistor 56, and thereby prevents the AC motor 40 from being damaged and from rotating by external forces to enable the AC motor 40 to make a quick stop.

[0054] The control part controls the on-off interval of the control switching element 58 and has a same effect as a variable resistor 70 (refer to FIG. 8C and 9).

[0055] As shown in FIGS. 8A-8B, the faster the AC motor 40 rotates, the shorter a turn-on time (T_{on}) of the control switching element 58, and the slower the AC motor 40 rotates, the longer the turn-on time (T_{on}) of the control switching element 58. Hence, when a speed of the AC motor 40 increases, a duty ratio ($D = T_{on}/T_s$) of the control switching element 58 decreases, and when the speed of the AC motor 40 decreases, the duty ratio ($D = T_{on}/T_s$) increases.

[0056] The current flowing in the winding wires around the AC motor 40 flows through the braking resistor 56, the over voltage protection resistor 54, and the control switching element 58. Since the duty ratio of the control switching element 58 varies depending on the speed of the motor 40, the braking resistor 56, the over voltage protection resistor 54, and the control switching element 58 operates together like that of a single variable resistor 70, as shown in FIG. 8C.

[0057] A value of the variable resistance is a same as a value of a compound resistance ($R_D||R_{ov}$) formed by a parallel connection between the braking resistor 56 and the over voltage protection resistor 54 divided by the duty ratio (D) of the control switching element 58. A value of the braking resistance (R_D) is comparatively smaller than a value of the over voltage protection resistance (R_{ov}), thus the value of the compound resistance ($R_D||R_{ov}$) is close to the value of the braking resistance (R_D). Therefore, the value of the variable resistance is similar to a ratio of the value of the braking resistance (R_D) to the duty ratio (D). When the speed of the

AC motor 40 increases, the duty ratio (D) decreases to increase the value of the compound resistance, and when the speed of the AC motor 40 decreases, the duty ratio (D) increases to decrease the value of the compound resistance.

[0058] Thus, if the AC motor 40 makes a sudden stop or stops driving when power is not applied, the speed of the AC motor 40 becomes a variable to setup a satisfactory value of the braking resistor 56, and specifies the value if necessary to reduce a size of a PCB (Printed Circuit Board) and a size of product.

[0059] The composition of circuits may be simple since the control switching element 58 is useable for the over voltage protection and further useable for braking operations.

[0060] In the above-described embodiments, the motor power supply supplies power for a three-phase motor, but as can be appreciated by one of ordinary skilled in the art, a number of phases of the motor is not limited three but may vary by changing a structure of the inverter 30.

[0061] With this configuration, a motor power supply is provided in which a number of elements is reduced by sharing a diode between a dynamic braking circuit and an inverter and, further, a size of a product and a manufacturing expense thereof are reduced. Further, with an effect that a value of resistance in a braking mode is variable depending on the motor speed, a satisfactory value of resistance for a braking circuit is provided.

[0062] Although an embodiment of the present invention has been shown and described, it will be appreciated by those skilled in the art that changes may be made in the embodiment without departing from the principles and spirit of the invention, the scope of which is defined in the appended claims and their equivalents.

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